

Hybrid H-mode scenario with nitrogen seeding and Type III ELMs in JET

Y. Corre¹, E. Joffrin¹, P. Monier-Garbet¹, Y. Andrew², G. Arnoux¹, S. Brezinsek³, M. Brix², R. Buttery², I. Coffey⁴, K. Crombe⁵, E. De La Luna⁶, R. Felton², C. Giroud², S. Hacquin¹, J. Hobirk⁷, A. Huber³, F. Imbeaux¹, S. Jachmich⁸, M. Kempenaars², H. Leggate², T. Loarer¹, G. Maddison², E. Rachlew⁹, J. Rapp³, O. Sauter¹⁰, A. Savchkov², F. Tabares⁶, G. Telesca³, A. Widdowson³, K. D. Zastrow², O. Zimmermann³ and JET-EFDA collaborators*

1) Association Euratom-CEA, CEA/DSM/DRFC, 13108 Saint-Paul-Lez-Durance, France

2) EURATOM/UKAEA Association, Culham Science Centre, Abingdon OX14 3DB, UK

3) Institut für Energieforschung – Plasmaphysik, Forschungszentrum Jülich GmbH, EURATOM-Assoziation, Trilateral Euregio Cluster, D-52425 Jülich, Germany

4) Queen's University, Belfast, BT7 1NN, UK

5) Department of Applied Physics, Ghent University, Rozier 44, B-9000 Ghent, Belgium

6) EURATOM-CIEMAT, Laboratorio Nacional de Fusion. Spain

7) Max-Planck Institut fuer Plasmaphysik, EURATOM Association, Garching, Germany

8) Association EURATOM-Belgian State, KMS-ERM B-1000, Brussels, Belgium

9) Association EURATOM-VR, KTH Roy. Inst. of Tech., SE-10691 Stockholm, Sweden

10) Association EURATOM Confédération Suisse, CRPP - EPFL, 1015 Lausanne, Switzerland

* See the Appendix of M.L. Watkins et al., Fusion Energy 2006 (Proc. 21st Int. Conf. Chengdu) IAEA

1. Introduction.

The performance of the hybrid H-mode regime has been extensively investigated in JET experiments up to $\beta_N=3$, toroidal field $B_t=1.7T$, with type I ELMs edge conditions. The optimized external current drive sources and stability properties in the plasma core provide a good prospect of achieving a high fusion gain at reduced plasma current for durations up to 2000 s in ITER [1]. One of the remaining issues is the problem of erosion of the divertor target plates associated with the type I ELM regime. A possible solution could be to operate with a plasma edge in the type III ELM regime (reduced heat loads) obtained with impurity seeding [2]. In this paper we report on experiments that have recently been performed on JET to investigate the feasibility of an integrated hybrid type III ELM regime with nitrogen seeding.

2. Description of the hybrid type III ELM scenario.

Experimental scenario: The target plasma is a hybrid H-mode with type I ELMs ($T_{ped}\sim 1000eV$), $I_p=1.7MA$, $q_{95}\sim 3.2$ in which NBI injection is feedback controlled to $\sim 18-20MW$ to achieve $\beta_N=2.6$. A high triangularity magnetic configuration ($\delta=0.44$) is used with MkII-HD divertor (with horizontal septum replacement plates). Nitrogen is injected into the private-flux zone of the divertor (from the horizontal target plate located on the high field side – GIM11). Nitrogen is chosen because it radiates at low plasma temperature, mainly in the divertor and pedestal region. Lower hybrid heating is used during the plasma current ramp up (during $\sim 3s$) to delay the penetration of the plasma current density towards the plasma core with the aim of broadening the q profile when the main heating is applied. This is followed by

an intermediate $\beta_N = 2$ phase (during ~ 3 s) for stabilization of the q-profile close to 1 in order to stabilize the MHD. The β_N request is then increased during 4 seconds ($\beta_N = 2.6$ has been obtained with high deuterium fuelling and $n_e \sim 0.95 \cdot n_{Gr}$). During this phase, a pre-set injection of deuterium is applied in the bottom of the divertor (on the low field side – GIM9). Nitrogen injection is applied during the first three seconds of the $\beta_N = 2.6$ plateau.

Hybrid type I and III ELM scenarios: The transition from type I to a stationary type III ELM regime has been obtained with radiative feedback control on the bolometric signals. The maximum radiated power fraction achieved with deuterium fuelling alone is $P^{rad}/P^{tot} \sim 35\%$. Using deuterium plus nitrogen fuelling enables to increase the radiative fraction up to 50%. This value is obtained by using the baseline of the bolometer signals, which represents the level of radiation *in between* ELMs. The type III ELM regime, characterized by the ELM frequency and amplitude, is achieved when $f^{rad} > 40\%$. Fig. 1 shows the hybrid type III ELM regime compared to the reference hybrid scenario with high D-fuelling.

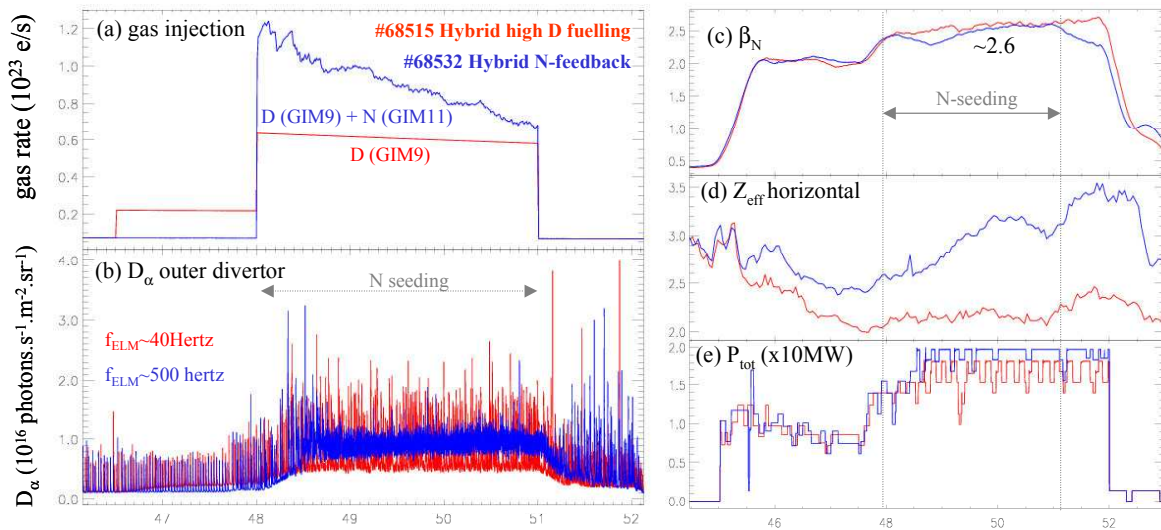


Figure 1: (a) gas fuelling. (b) D_α signal in the outer divertor. (c) β_N . (d) Z_{eff} from visible spectroscopy (horizontal channel). (e) neutral beam power for the reference type I and type III ELM regimes.

A strong gas puff ($\Phi_D = 5 \times 10^{22}$ e/s and $\Phi_N \sim 7 \times 10^{22}$ e/s) is required to cool the pedestal and reach the type III ELM regime. This phase is followed by a moderate and decreasing impurity fuelling ($\Phi_N \sim 3 \times 10^{22}$ e/s) to maintain the regime stationarity. The total radiated power fraction achieved with the type III ELM regime is $\sim 50\%$ with $\beta_N = 2.6$ ($P_{NBI} \sim 20-22$ MW) and a thermal confinement factor of $H_{98}^*(y,2) \sim 0.83$. The MHD activity is characteristic of that observed in standard hybrid scenario (no strong MHD and reduced sawtooth activity). Note that $n=1$ sawtooth precursors are present during the seeding phase, which means q_{min} is equal

5) Hybrid type III ELM performance: The hybrid type III ELM scenario using N-seeding has been successfully developed in JET with $I_p=1.7\text{MA}$, $q_{95}\sim 3.2$, $n_e\sim 0.95\cdot n_{Gr}$, $\beta_N\sim 2.6$. The plasma performance of this scenario is described by the global energy confinement factor $H_{98(y,2)}$ presented in Fig. 3 as a function of the radiated fraction for a series of hybrid discharges with D-fuelling and a mixture of D+N fuelling. The contribution of fast particles has been subtracted in order to identify the thermal part of the confinement. With pure deuterium fuelling, the standard H-mode behaviour is observed: at low-D fuelling (#68505) the hybrid discharges fulfil the ITER confinement requirements when high-D fuelling is accompanied by a net reduction of the global confinement: $\sim 10\%$ losses with $\Phi_D=5\cdot 10^{22}$ e/s (#68515) and $\sim 20\%$ losses with $\Phi_D=9\cdot 10^{22}$ e/s (#68739) without significant increase of the radiated fraction. N-seeding does not modify significantly the global energy confinement but enables to reach higher radiated fraction. The degradation of global confinement associated with the type III ELM regime is about 10% compared to the reference hybrid high D-fuelling discharge (#68515), which uses the same D-fuelling: $\Phi_D=5\cdot 10^{22}$ e/s. The integrated hybrid type III ELM scenario shows good edge plasma conditions (reduced heat loads and erosion) with moderate MHD activity (q_{\min} close to unity). Although this scenario does not fulfill the ITER requirements ($H_{98(y,2)}^*\sim 0.83$), it is optimized for current drive sources due to high β_N operation and offers good prospects of achieving stable long discharges in ITER.

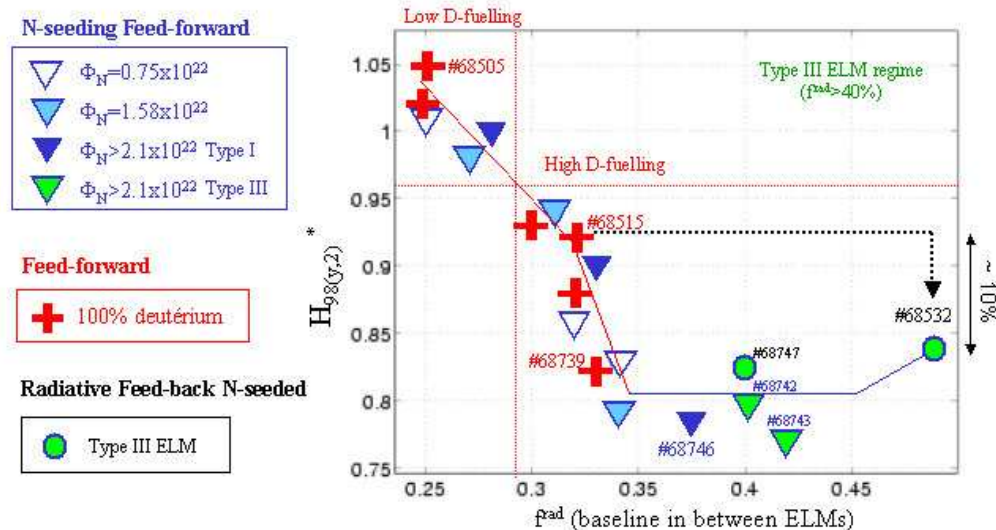


Figure 5: Thermal confinement enhancement factor $H_{98(y,2)}$ versus the radiated fraction measured in between ELMs for a series of pulses with D-fuelling only (red) and D+N fuelling (blue and green are associated with type I and III ELM regime respectively).

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