

## Equations of state for nickel, copper and zinc at high energy densities

K.V. Khishchenko

*Joint Institute for High Temperatures, Russian Academy of Sciences, Moscow, Russia*

A description of the thermodynamic properties of matter in a wide range of temperatures and densities is of both fundamental and practical interests. The equations of state (EOSs) for metals over the range from normal conditions to extremely high energy densities are required for numerical simulations of hydrodynamic processes in plasmas under pulsed power influences [1].

In this paper, a new semiempirical EOS model, which takes into account the melting, evaporation and ionization effects, is proposed.

The specific free energy of the substance is considered as a sum of three components [2],

$$F(V, T) = F_c(V) + F_a(V, T) + F_e(V, T), \quad (1)$$

describing the cold part of interparticle interaction at  $T = 0$  K ( $F_c$ ) and the thermal contributions by heavy particles (atoms, ions, nuclei) and electrons ( $F_a$  and  $F_e$  respectively). The first and second components of Eq. (1) have different forms for the solid and liquid phases, but the third is defined identically as in the EOS model [3].

The cold interaction energy for the solid phase is given by the relations [4]. The thermal lattice component of the free energy is defined as follows,

$$F_a(V, T) = RT \left( 3 \ln \left( 1 - e^{-\theta_a/T} \right) - D(\theta_a/T) \right), \quad (2)$$

where  $R = k_B (Am_u)^{-1}$ ,  $k_B$  is the Boltzmann constant,  $m_u$  is the atomic mass unit (amu),  $A$  is the atomic mass (in amu),  $D$  is the Debye function [5],  $\theta_a = \theta_s(V)$  is the characteristic temperature of phonon spectrum [3],

$$\theta_s(V) = \theta_{s0} \sigma^{2/3} \exp \left( (\gamma_{s0} - 2/3) \frac{B_s^2 + D_s^2}{B_s} \arctan \frac{B_s \ln \sigma}{B_s^2 + D_s (\ln \sigma + D_s)} \right), \quad (3)$$

where  $\sigma = V_0/V$ ,  $V_0$  and  $\gamma_{s0}$  are the values of specific volume and Grüneisen coefficient of the solid phase under normal conditions.

The energy of the liquid phase at  $T = 0$  K is determined by the relations

$$F_c^{(l)}(V) = F_c^{(s)}(V) + \frac{2\sigma_l^2}{1 + \sigma_l^3} \left( d_0 + \frac{d_n}{n_l} \sigma_l^{n_l} \right) \text{ at } \sigma_l \geq 1, \quad F_c^{(l)}(V) = \sum_{i=1}^3 \frac{d_i}{n_i} \sigma_l^{n_i} + E_{sub} \text{ at } \sigma_l < 1, \quad (4)$$

where superscripts  $s$  and  $l$  denote the solid phase and the liquid,  $\sigma_l = V_{l0}/V$ ,  $V_{l0}$  is the specific volume of the liquid phase at a chosen point on the melting curve ( $P = P_{m0}$ ,  $T = T_{m0}$ ), the

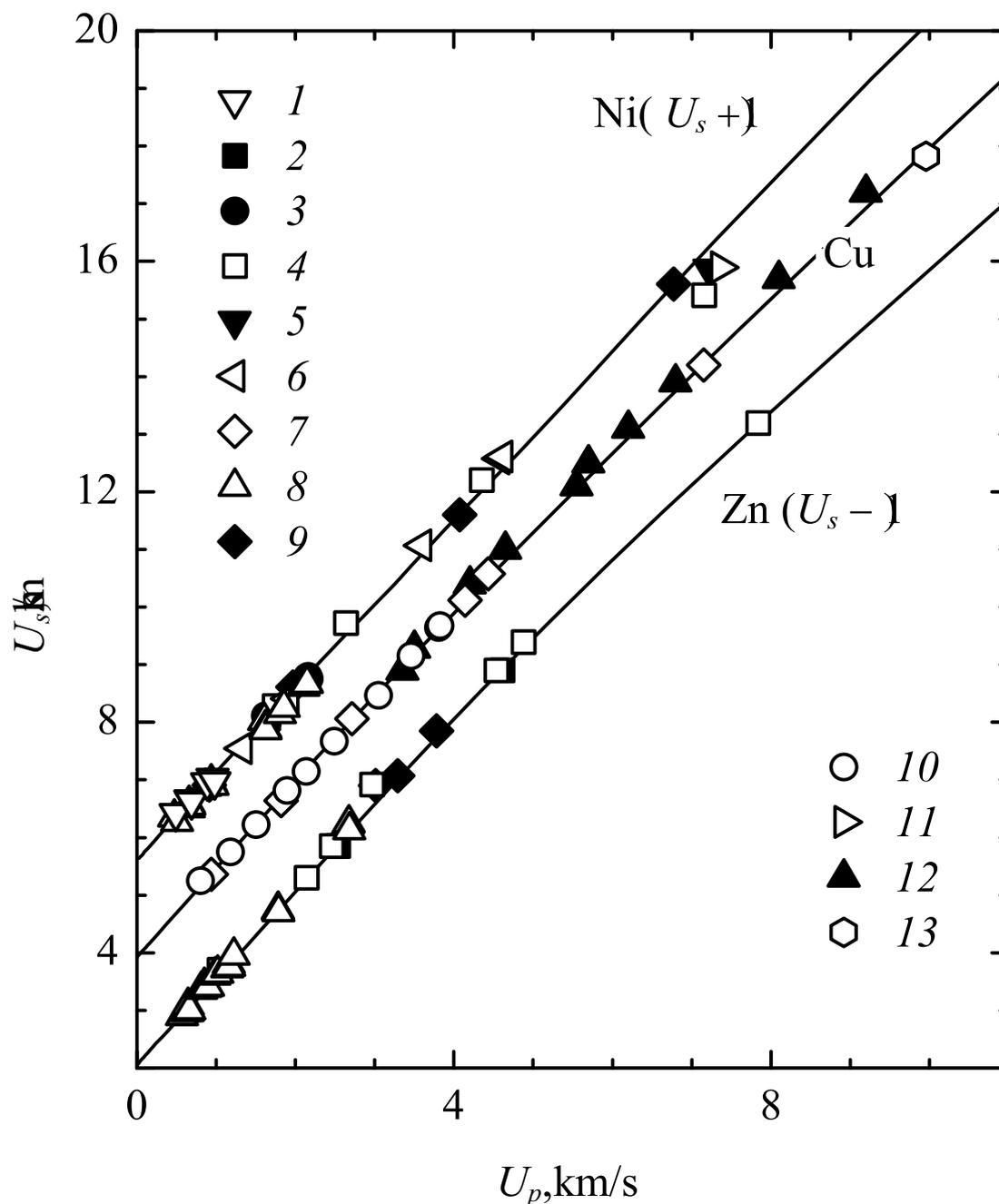


Figure 1: Shock velocity ( $U_s$ ) versus particle velocity ( $U_p$ ) on the Hugoniots of nickel, copper and zinc. Experimental data: 1 — [6], 2 — [7], 3 — [8], 4 — [9], 5 — [10], 6 — [11], 7 — [12], 8 — [13], 9 — [14], 10 — [15], 11 — [16], 12 — [17], 13 — [18].

coefficients  $d_0$  and  $d_n$  define the volume change under melting at this point,  $E_{sub}$  is the sublimation energy. The parameters  $d_i$  and  $n_1$  are determined from the requirement of continuity of the function (4) and its three derivatives with respect to volume at  $\sigma_l = 1$ .

The contribution of thermal movement of heavy particles to the free energy of the liquid

phase is defined in the form of Eq. (2), where  $\theta_a = \theta_l(V) + (T_a T \sigma_l^{2/3})^{1/2}$ ,  $T_a$  is a constant,

$$\theta_l(V) = \theta_{l0} \sigma_l^{2/3} \exp \left( (\gamma_{l0} - 2/3) \frac{B_l^2 + D_l^2}{B_l} \arctan \frac{B_l \ln \sigma_l}{B_l^2 + D_l (\ln \sigma_l + D_l)} \right), \quad (5)$$

the parameter  $\theta_{l0}$  defines the enthalpy change under melting at  $P = P_{m0}$ ,  $\gamma_{l0}$  is the value of Grüneisen coefficient of the liquid phase at  $\sigma_l = 1$ .

Wide-range EOSs for nickel, copper and zinc are constructed on the basis of model developed. Calculation results are compared with available experimental data at high temperatures and pressures. The most essential shock-wave experiments [6–18] are described, see Fig. 1. The EOSs obtained can be used efficiently in numerical simulations of different processes at high energy densities.

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