

## COMPUTATIONAL STUDIES FOR FAST HEATING IN FIREX-I

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### 1. Introduction

On the fast ignition integrated experiments for cone-guided CD targets with GekkoXII+PW laser systems [1], the efficient heating of imploded cores ( $\sim 800\text{eV}$ ) was demonstrated, where the implosion laser was operated with the energy of 2.5kJ and the duration of 1.2ps (flat top) and the heating laser was operated with the power of 0.5PW and the duration of 0.6ps (the Gaussian). As the next step, FIREX (Fast Ignition Realization EXperiment) project [2] has been started. In the phase I (FIREX-I), a foam-cryogenic DT target is imploded by the GekkoXII laser operated with higher energy mode and the imploded core is heated by the 10kJ LFEX laser. The goal of FIREX-I is the core heating up to ion temperature of  $\sim 5\text{keV}$ . From the previous experiments, the heating laser energy and duration, the implosion laser energy and the fuel material are different in FIREX-I. In the present study, on the basis of core heating simulations for pre-compressed core plasmas, we evaluate those effects and show the requirement for achieving the goal of FIREX-I, 5keV heating.

### 2. Simulation Model

The 2D core heating simulations were carried out using "FIBMET" [3], which is based on 1-fluid 2-temperature Eulerian hydrodynamic code written in 2D cylindrical coordinates ( $r - z$ ) with axial symmetry. In this code, the Thomas-Fermi model and the Cowan model are adopted for the equations of states of electron and ion, respectively. In the energy conservation equation, electron thermal conduction, radiation effect, alpha-particle heating and external fast electron heating are taken into account. The radiation and alpha-particle transports are treated by multi-group diffusion models. As for the core heating process, we assumed the uniform heating rate per particle for the bulk electron. Uniformly-compressed stationary plasma spheres are assumed as imploded core profiles. The spatially-uniform temperature ( $T_i = T_e = 0.35\text{keV}$ ) is assumed and the Gaussian profile is assumed for the radial profile of density.

### 3. Core Heating Properties in CD Core

First, we evaluated the effect of increase in heating energy  $E_h$  by assuming a CD core, of which density at the centre  $\rho_0$ , and mass  $M_f$  are set so as to reproduce the neutron yield and heated core temperature measured at the previous GEKKO XII+PW experiments [1];  $\rho_0 = 100\text{g/cm}^3$ ,  $M_f = 0.0015\text{mg}$ , the areal density  $\rho_0 R_0 = 0.13\text{g/cm}^2$  ( $R_0$  is the initial core radius) and the internal energy  $E_{\text{int}} = 50.1\text{J}$ .

Figure 1 shows the heating energy dependences of the DD neutron yield  $Y_{\text{DDn}}$  and the average temperatures of electron and ion weighted with DD fusion reaction rates  $\langle T_e \rangle_{\text{DDn}}$ ,

$\langle T_i \rangle_{\text{DDn}}$ . When  $E_h \leq 100\text{J}$ , we assumed the Gaussian pulse (FWHM = 600fs) for heating pulse, which corresponds to the PW laser pulse shape at the previous experiments. When  $E_h \geq 0.5\text{kJ}$ , a 10ps flat pulse was assumed, which corresponds to the LFEX laser pulse shape. In the case of heating energy of 40~80J,  $\langle T_i \rangle_{\text{DDn}}$  of ~800eV and  $Y_{\text{DDn}}$  of  $\sim 10^7$  are obtained. If the energy coupling from heating laser to core  $\eta_h$  is 20%, the heating laser energy becomes 200~400J. These values well agree with those at the previous experiments.

When the heating pulse is assumed as 0.5~5kJ / 10ps,  $\langle T_e \rangle_{\text{DDn}}$  monotonically increases with  $E_h$ . The bulk ion is heated through the temperature relaxation between electron and ion, and then  $\langle T_i \rangle_{\text{DDn}}$  is lower than  $\langle T_e \rangle_{\text{DDn}}$ . In addition,  $\langle T_i \rangle_{\text{DDn}}$  reaches a peak at  $E_h = 3\text{kJ}$ , and it decreases with increasing  $E_h$  in the higher energy region. The same tendency is observed in  $Y_{\text{DDn}}$ . The size of core generated by the present implosion laser is so small that the confinement time is short, and then the core is rapidly disassembled due to the heated electron pressure. In the case of such a small-sized core, hence, the excessive heating of the bulk electron leads to the rapid core disassembly before the ion is sufficiently heated. In the case of CD core of which size is the same as that generated at the previous experiments, the goal of FIREX-I,  $\langle T_i \rangle = 5\text{keV}$ , is achieved with  $E_h > 2\text{kJ}$ , which means that  $\eta_h > 20\%$  is required. The required value for  $\eta_h$  is already realized at the previous experiments, where the estimated value of  $\eta_h$  was  $\sim 20\%$  [1].

The GEKKO XII implosion laser will be operated with higher energy mode in FIREX-I than that at the previous experiments. Thus, the fuel mass and the imploded core density are expected to be larger, which leads to increase in the ion heating efficiency. We carried out the simulations for a larger and denser CD core ( $M_f = 0.002\text{mg}$ ,  $\rho_0 = 200\text{g/cm}^3$ ,  $\rho_0 R_0 = 0.22\text{g/cm}^2$  and  $E_{\text{int}} = 84\text{J}$ ). Since the number of electrons in the core increases with increasing fuel mass, the heating rate per electron and the resultant electron temperature become low for a given  $E_h$ . In Fig.2,  $E_{\text{ei}}/E_h$  and  $\langle T_i \rangle_{\text{DDn}}$  are plotted as a function of  $E_h$ , where  $E_{\text{ei}}$  is the energy transferred from electron to ion due to the relaxation process. Because of high density,  $E_{\text{ei}}/E_h$  is higher in the denser core. In the low heating energy region ( $E_h < 3\text{kJ}$ ),  $\langle T_i \rangle_{\text{DDn}}$  in the case of the large and dense core is lower because of the low  $\langle T_e \rangle_{\text{DDn}}$  (a defect of increase in mass). In the high heating energy region ( $E_h > 3\text{kJ}$ ), the density effect (*i.e.*, increases in  $E_{\text{ei}}/E_h$ ) overcomes the defect of

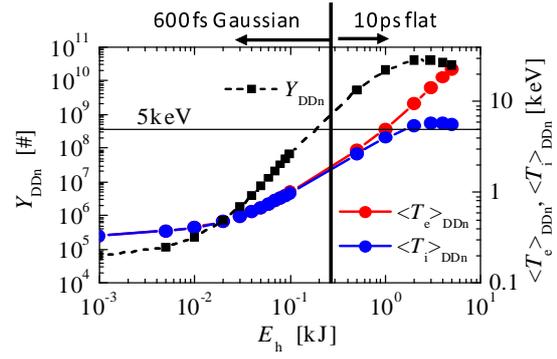


Fig.1  $Y_{\text{DDn}}$ ,  $\langle T_e \rangle_{\text{DDn}}$  and  $\langle T_i \rangle_{\text{DDn}}$  as a function of heating energy  $E_h$  in the case of a CD core with  $M_f = 0.0015\text{mg}$ ,  $\rho_0 = 100\text{g/cm}^3$ .

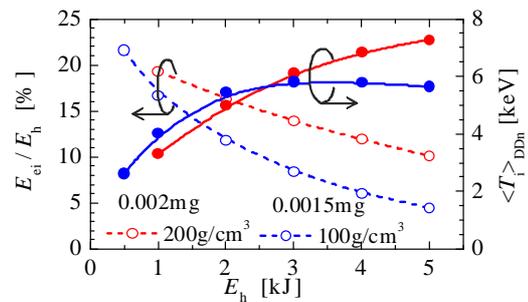


Fig.2  $E_{\text{ei}}/E_h$  and  $\langle T_i \rangle_{\text{DDn}}$  in the different-sized CD cores as a function of  $E_h$ .

increase in mass, and then  $\langle T_i \rangle_{\text{DDn}}$  becomes higher in the case of the large and dense core.

The increase in  $\rho_0 R_0$  enhances the energy coupling from fast electron to core,  $\eta_{\text{fe} \rightarrow \text{core}}$ . In dense plasmas, the Coulomb interactions with bulk electrons are the dominant mechanism in the fast electron energy deposition process [4,5]. The collisional stopping power is proportional to the bulk electron number density  $n_e$ , and then the optical thickness of a dense core for fast electrons is roughly estimated by  $2n_e R$  ( $R$  is the core radius). Thus,  $\eta_{\text{fe} \rightarrow \text{core}}$  will increase by  $\sim 70\%$  when the  $\rho_0 R_0$  increases from  $0.13 \text{g/cm}^2$  to  $0.22 \text{g/cm}^2$ .

In the case of the CD target, therefore, achievement of  $\langle T_i \rangle_{\text{DDn}} = 5 \text{keV}$  in FIREX-I can be extrapolated on the basis of the imploded core parameters and  $\eta_h$  obtained at the previous experiment. By operating implosion laser with higher energy mode to implode a larger target and compress it into higher density than those at the previous experiments, the ion heating efficiency becomes higher, and then achievement of  $\langle T_i \rangle_{\text{DDn}} = 5 \text{keV}$  will be more promising.

#### 4. Core Heating Properties in DT core

For a fixed mass and density, the optical thickness of a core for fast electron is proportional to  $n_e \propto Z/A$  ( $Z$  and  $A$  are the effective charge and mass number of fuel ion). Compared with a CD fuel, a DT fuel is optically thin for fast electrons by 20%, and then the energy coupling from fast electron to core will lower in the DT core. In addition, since the electron-ion temperature relaxation time  $\tau_{ei}$  is proportional to  $A/\langle Z^2 \rangle$ , the ion heating rate is lower in the DT fuel. Thus, the ion heating in the case of the DT fuel is inefficient compared with the CD fuel.

In Fig.3,  $\langle T_i \rangle_{\text{DDn}}$  for the CD core and  $\langle T_i \rangle_{\text{DT}}$  for the DT core are plotted as a function of  $E_h$ , where  $M_f = 0.002 \text{mg}$ ,  $\rho_0 = 200 \text{g/cm}^3$  and  $\rho_0 R_0 = 2.2 \text{g/cm}^2$  for both fuels and  $E_{\text{int}} = 114 \text{J}$  for the DT core.  $\langle T_i \rangle_{\text{DT}}$  is a DT reaction rate weighted average ion temperature. (Noted that to achieve the same density, five times higher compression from the solid state is required in the DT fuel.) To achieve the average ion temperature of  $5 \text{keV}$ , the higher heating energy is required in the case of DT core, *i.e.*,  $E_h > 3 \text{kJ}$  ( $2 \text{kJ}$ ) is required in the DT (CD) case. Thus, the requirements for implosion and heating in a DT fuel are more severe than those in a CD fuel.

In Fig.4,  $\langle T_i \rangle_{\text{DT}}$  in the case of the  $0.002 \text{mg}$  DT fuel as a function of  $E_h$ ,  $\tau_h$  and  $\rho_0$ , where  $\tau_h$  is the duration of heating pulse. There exists an optimum value of  $\tau_h$  to maximize  $\langle T_i \rangle_{\text{DT}}$  for a given  $\rho_0$  and  $E_h$ ; it becomes long with increasing  $E_h$  and short with increasing  $\rho_0$ . With increasing density, the relaxation time becomes short, and then  $\langle T_i \rangle_{\text{DT}}$  increases. To achieve  $\langle T_i \rangle_{\text{DT}} = 5 \text{keV}$  using DT fuels,  $\rho_0 > 200 \text{g/cm}^3$  (that is 1000 times solid density) is required. As for the heating parameters,  $\tau_h = 2 \sim 5 \text{ps}$  ( $2 \sim 10 \text{ps}$ ) is required in the case of  $\rho_0 = 200 \text{g/cm}^3$  with  $E_h = 2 \text{kJ}$  ( $3 \text{kJ}$ ) heating.

We also evaluated the effect of the foam material [6]. To achieve the ignition and burning, the required mass density of foam in the solid state is less than  $20 \text{mg/cm}^3$  [7] since the foam material increases the radiation loss

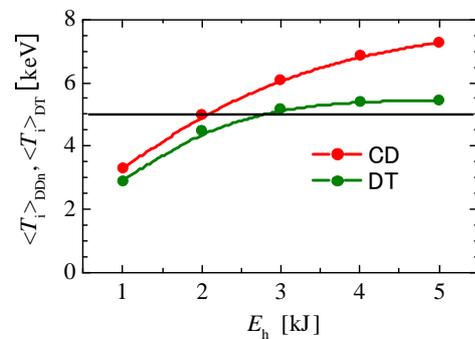


Fig.3  $\langle T_i \rangle_{\text{DDn}}$  for the CD core and  $\langle T_i \rangle_{\text{DT}}$  for the DT core as a function of  $E_h$ , where  $M_f = 0.002 \text{mg}$  and  $\rho_0 = 200 \text{g/cm}^3$ .

from the heated region. However, in the FIREX-I class targets, the core is heated only by the external source and the core temperature rapidly decreases after finishing external heating due to the core disassembly since the core size is small. Under this situation, a small amount of foam material contribute to suppress the excessive increase in bulk electron temperature and to enhance the energy relaxation between bulk electron and ion. We found that when the density of foam material in the solid state is lower than  $100\text{mg}/\text{cm}^3$ , the obtained  $\langle T_i \rangle_{\text{DT}}$  is higher than that in the pure DT case.

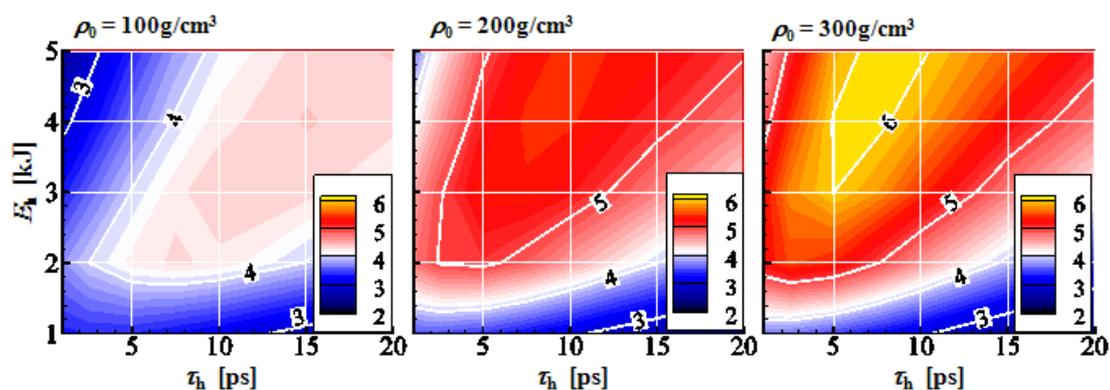


Fig.4  $\langle T_i \rangle_{\text{DT}}$  in the case of the 0.002mg DT fuel as a function of  $E_h$ ,  $\tau_h$  and  $\rho_0$ .

## 5. Conclusion

On the basis of core heating simulations for the FIREX-I class CD and DT cores, we showed the importance of temperature relaxation between the bulk electron and ion. It is found that compared with the CD core, requirement for implosion and heating to achieve the core temperature of 5keV (the goal of FIREX-I) is severe in the DT core. The required condition for 5keV ion heating in the DT core is the core density  $> 200\text{g}/\text{cm}^3$ , the core heating energy  $> 2\text{kJ}$  ( $> 20\%$  coupling from 10kJ LFEX laser) and heating duration  $< 10\text{ps}$ .

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## References

- [1] R. Kodama, *et al.*, Nature 418, 933 (2002).
- [2] K. Mima, Annual Progress Rep. 2001 (Institute of Laser Engineering, Osaka University, 2001) p.1.
- [3] T. Johzaki *et al.*, Proc. of IFSA2003, Monterey, CA, 2003 (American Nuclear Society, 2004) p.474.
- [4] T. Johzaki, *et al.*, Fusion Sci. Technol. 43, 428 (2003).
- [5] A. J. Kemp, *et al.*, Phys. Rev. Lett. 97, 235001 (2006).
- [6] F. Ito *et al.*, Jpn. J. App. Phys. 45, L335 (2006).
- [7] T. Johzaki, *et al.*, "Simulation Study on Ignition and Burn Characteristics of Fast Ignition DT Targets", submitted to Plasma and Fusion Research.