

## Predictive simulation of tokamak discharge behaviour based on simple scalings

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### Introduction

The operation of tokamak experiments can be facilitated by control room tools that predict the plasma discharge behaviour based solely on machine parameters and requested waveforms of coil currents, gas puff, etc. We describe here a publicly available simulation toolkit fully based on open source software that implements a variety of models which are based on simple physics relations. These are obtained from empirical scalings of the plasma density, the confinement time etc. and allow to predict basic properties of a tokamak discharge like actual plasma density, stored energy, ohmic transformer flux consumption and transition times to and from high-confinement mode (H-mode). The data described is from the ASDEX Upgrade tokamak, however the tools can be ported relatively easily to other machines.

### Experimental data base

In the context of the present model, tokamak transport physics is described in terms of scalar quantities. For ASDEX Upgrade, four data sets are used to determine parameter dependencies: 803 stationary ELMy H-mode phases selected for largest variation of engineering parameters  $B_t$ ,  $I_p$ ,  $P_{\text{heat}}$ , gas puff and plasma shaping (triangularity). 416 phases from the ASDEX Upgrade contribution to the international confinement database, 916 phases (H-mode) and 386 phases (L-mode) have been compiled to map out operational regime boundaries.

The central line-averaged plasma density  $\bar{n}_e$  can be feedback-controlled, or result from a prescribed gas fuelling rate in the divertor or in the main chamber ( $\Gamma_{0,\text{div}}$ ,  $\Gamma_{0,\text{main}}$ , both in atoms/second). Alternatively, the neutral gas density in the divertor  $n_{0,\text{div}}$  or main chamber  $n_{0,\text{main}}$  can be feedback controlled. It is assumed that in steady state the controlled quantities are actually obtained. The plasma density  $\bar{n}_e$  is approximated by a power law  $\bar{n}_e = A \prod_i Q_i^{\alpha_i}$  with the prefactor  $A$  and exponents  $\alpha_i$  obtained by log-linear regression (table 1).

The plasma shape dependence of the density scaling is expressed through the upper triangularity  $\delta_u$ . The lower triangularity is strongly correlated with  $\beta_p$  and therefore less suitable. In the currently implemented models, the Grad-Shafranov equation is not solved. Instead,  $\delta_u$  is obtained by linear regression of shaping coil currents and  $I_p$  (Fig. 1, rms error 17.9%).

The energy confinement time ( $\tau_{\text{tot}} = W_{\text{tot}}/P_{\text{heat}}$ ), L-H and H-L transition power thresholds ( $P_{\text{L}\rightarrow\text{H}}$ ,  $P_{\text{H}\rightarrow\text{L}}$ ) and minimum (“natural”) H-mode density are determined by scalings with engineering parameters and  $\bar{n}_e$ . Finally, the core radiated power  $P_{\text{rad}}$  and plasma resistance  $R$  depend on plasma temperature which is approximated by a dependence on  $W_{\text{tot}}$  and  $\bar{n}_e$ . A list of scaling coefficients is given in table 2.

### Implementation

The temporal discharge behaviour is described by sets of coupled ordinary differential equations. They are integrated in time using the Scicos simulation toolkit ([www.scicos.org](http://www.scicos.org)), distributed as part of the Scilab mathematical package ([www.scilab.org](http://www.scilab.org)). Several models with

Table 1: Scalings of  $\bar{n}_e$  as a function of  $n_{0,main}$ ,  $n_{0,div}$ ,  $\Gamma_{0,main}$ ,  $\Gamma_{0,div}$  for H-mode and L-mode

prefactor $10^{19}m^{-3}$	$I_p$ MA	$B_t$ T	$P_{tot}$ MW	$0.1 + \delta_u$	$n_{0,main}$	$n_{0,div}$	rmse %
H-mode							
14.60	$1.04 \pm 0.02$	$-0.45 \pm 0.02$	0	$0.12 \pm 0.01$	$0.11 \pm 0.01$		15.2
7.701	$1.08 \pm 0.05$	$-0.30 \pm 0.04$	$-0.14 \pm 0.02$	$0.11 \pm 0.01$		$0.15 \pm 0.01$	13.2
					$\Gamma_{0,main}$	$\Gamma_{0,div}$	
					$10^{21}m^{-3}s^{-1}$		
11.68	$1.07 \pm 0.05$	$-0.42 \pm 0.05$	0	$0.08 \pm 0.01$	$0.08 \pm 0.01$		14.2
9.403	$1.00 \pm 0.11$	$-0.60 \pm 0.09$	$0.20 \pm 0.04$	$0.04 \pm 0.01$		$0.05 \pm 0.01$	11.1
L-mode							
					$n_{0,main}$	$n_{0,div}$	
14.84	$0.64 \pm 0.07$	$-0.41 \pm 0.06$	$0.11 \pm 0.02$	$0.30 \pm 0.03$	$0.16 \pm 0.01$		17.4
4.833	$1.78 \pm 0.21$	$0.82 \pm 0.09$	$0.10 \pm 0.03$	0		$0.10 \pm 0.03$	9.4
					$\Gamma_{0,main}$	$\Gamma_{0,div}$	
9.608	$0.13 \pm 0.12$	$-0.21 \pm 0.14$	$0.09 \pm 0.04$	$0.17 \pm 0.06$	$0.24 \pm 0.03$		17.9
8.780	0	$0.49 \pm 0.24$	$-0.13 \pm 0.08$	$0.56 \pm 0.12$		$-0.07 \pm 0.05$	7.2

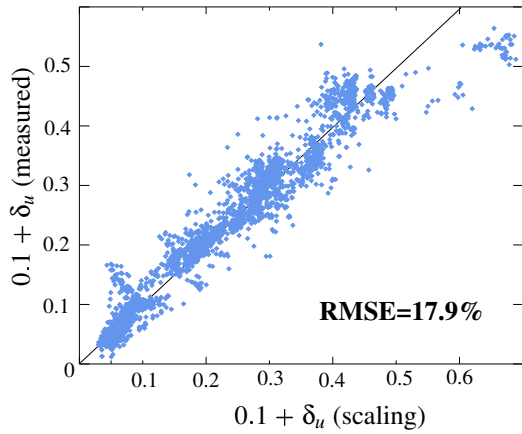


Figure 1: *Scaling of the upper triangularity*

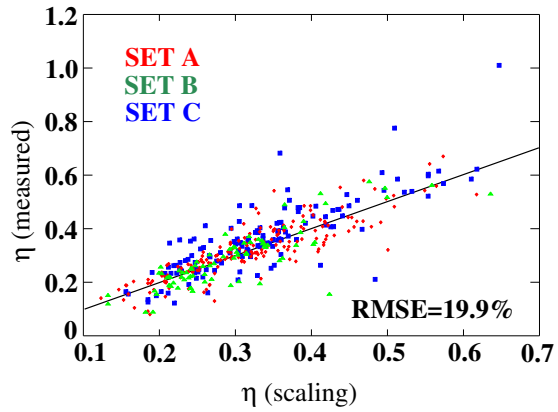


Figure 2: *Scaling of the plasma resistivity*

different complexity are available. Models are easily built by adding building blocks and logical connections to a diagram edited by a graphical user interface. Each simulation run is preceded by a data collection phase (machine dependent but model independent) and succeeded by a post-processing step to perform various consistency checks and issue warnings to the operator. The entire suite is controlled by an embracing Bourne shell script, which is called once per discharge and takes a few seconds to run. For waveform input and output, interface blocks to MDSplus ([www.mdsplus.org](http://www.mdsplus.org)) trees are implemented. The software described here is available for download at [www.ipp.mpg.de/~Wolfgang.Suttrop/mdsplus/tokfsim](http://www.ipp.mpg.de/~Wolfgang.Suttrop/mdsplus/tokfsim).

### Dynamical confinement model

Figure 3 shows the block diagram of a model for plasma density, stored energy, L-H/H-L transitions and ohmic flux consumption. The scalings for (reciprocal) confinement time, plasma

Table 2: Scalings of energy confinement time  $\tau_{tot}$ , L-H and H-L transition threshold powers  $P_{L \rightarrow H}$ ,  $P_{H \rightarrow L}$ , core radiated power  $P_{rad}$  and plasma resistance  $R$ .

quantity	units	prefactor	$I_p$	$B_t$	$P_{tot}$	$\bar{n}_e$	$(0.1 + \delta_u)$	$W_{tot}$	rmse
			MA	T	MW	$[10^{19} \text{ m}^{-3}]$		MJ	%
H-mode									
$\tau_{tot}$	s	0.75	1.43	-0.27	-0.62	-0.23	0.12		14.6
			$\pm 0.03$	$\pm 0.03$	$\pm 0.01$	$\pm 0.02$	$\pm 0.01$		
$P_{H \rightarrow L}$	MW	0.28		0.56		0.79			
$P_{rad}$	MW	0.017			0.080	1.38		-0.06	35.2
					$\pm 0.05$	$\pm 0.07$		$\pm 0.07$	
$R$	$\mu\Omega$	0.02				0.78		-1.16	19.9
						$\pm 0.04$		$\pm 0.04$	
L-mode									
$\tau_{tot}$	s	0.16	0.69	0.33	-0.53		0.20		16.7
			$\pm 0.07$	$\pm 0.05$	$\pm 0.02$		$\pm 0.03$		
$P_{L \rightarrow H}$	MW	0.51		0.56		0.79			

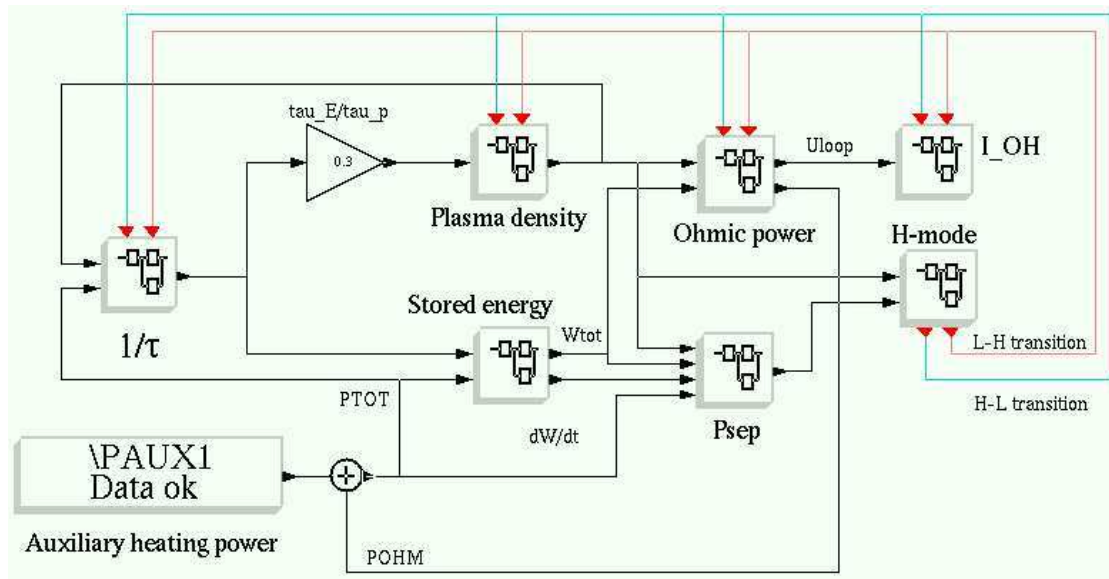


Figure 3: Scicos model for L- and H-mode plasma density, stored energy and ohmic transformer flux consumption.

density, plasma resistivity, radiated power and H-mode threshold power are used in the blocks labelled “ $1/\tau$ ”, “plasma density”, “Ohmic power”, “ $P_{sep}$ ” and “H-mode”, respectively. These blocks are nested models and edited in separate Scicos sheets. This block hierarchy allows to maintain a clear structure in more complex models. The ohmic transformer current (block “I-OH”) is integrated from the loop voltage using 3 fixed values of the plasma inductance at start-up, in L-mode and in H-mode and the scaling for plasma resistance. Variations of the poloidal field coil currents are taken into account by means of pre-calculated fixed values for their mutual inductances with the plasma column. The L-H and H-L transition is detected

